

Conceptual Design of CFETR Blanket Design (I): Solid Blanket

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What's Blanket Type is Suitable for CFETR?

- Tritium breeding blanket is a very complex component, work at very severe working condition. The concept of blanket will give the reactor's basic characteristics.
- It was assumed that CFETR should be steady state D-T operation, tritium selfsufficiency, and with net power output.
- Main design objectives will be:
 - to validate the tritium breeding performance , (TBR>1).
 - to realize the heat remove.
- Basic considerations for CFETR blanket selection:
 - Flexibility
 - Maintainability
 - Replaceability
 - Low-risk, and
 - Matured technology .

 Based on current mission and Chinese ITER TBM development strategy, two kinds of blanket concept options can be considered:

Option I: Helium-cooled ceramic tritium breeder with RAFM, HCCB;

Option II: Liquid Li-Pb tritium breeder with RAFM, DCLL;

It is very important that exiting technology foundation and abundant data bases.



General Consideration of Solid Breeder Blanket

Option (I) : Solid Breeder Blanket

The ceramic breeder blanket with RAFM material concept might be primary option for CFETR design. General consideration of solid blanket as the following:

- It is easy to realize blanket flexibility, maintainability, replaceability, and multifunction based on the modularized structure design.
- Solid blanket concept is current main stream design in ITER TBM program.
 - good tritium breeding and release performance.
 - widely TBR design margin (TBR from 1.0 to 1.22 with Be, depend on the calculation model, nuclear data, and design element, etc).
- Widely technology foundation and R&D data base on around the world.
- Without MHD, material corrosion and compatibility issues.
- Matured technology on tritium extraction, recovery, purification and processing.

Basic futures of solid breeder blanket

- Structure material: Reduced-activation Ferritic/Martensitic steel (RAFM)
- > Tritium breeder: Li_4SiO_4 or Li_2TiO_3 , with pebble bed structure.
- > Neutron Multiplier: Be, with pebble bed structure.
- Coolant: He gas with high pressure or supper-critical water coolant.
- Purge gas: He gas
- Tritium Breeding Rate: TBR >1.2



Parameter and Requirements

Assumed PI. Parameter Range

- Major radius: 4.9m,
- Minor radius: 1.2-1.5m
- Elongation : 1.75
- Triangularity: 0.4
- Neutron wall loading: 0.4-0.8MW/m²
- Fusion power : 200-400MW
- Operation duty : 0.3~0.5

Basic Requirements

- 1. Tritium Breeder: Ceramic Breeder, Li₄SiO₄ or Li₂TiO₃
- 2. Tritium Self-sufficiency (TBR>1.2, 3-D)
- 3. Blanket Thickness:_Breeding + Shielding + VV < 1.0 m
- 4. Replace is easy

Requirement of Tritium Breeder

- 1. High enrichment of ⁶LI: 80%-90%
- 2. High compatibility with structure materials and beryllium.
- 3. High heat, chemical, machinery and irradiation performance.
- 4. High tritium release performance.
- 5. Low tritium retention.
- 6. Tritium is easy to extract.



modularized blanket design





Structure and Materials of Blanket

 Single sized tritium breeder pebble Li₄SiO₄, D=1mm, packing rate is 60%, Concentration rate of ⁶Li > 80%.

Binary sized neutron mltiplier, Be pebble, D= 0.5-1.0mm, packing rate is 80%.
Thickness of each zones:

- First Wall: 3cm (structure material is RAFM).
- He cooling plate : 1cm.
- Shield zone : 30~50cm (depend on shield design).
- 5 lithium silicate zones: 6.4cm: 0.6, 1.0, 1.0, 1.3, 2.5cm.
- 4 beryllium zones : 25.1cm: 4.0, 5.0, 7.0, 10.1cm.



1-D Schematic of Outboard Blanket



Neutronics Analyses

Neutron Wall Loading Distribution

1-D Neutronics Code: ONEDANT/ANISN

- 3-D Neutronics Code Neutronics : MCNP, MCNPX Shielding : MCNP+TORT, FISPACT
- Nuclear Data Library: FENDL21

✓ Isotropic volume neutron source distribution ;

✓ The maximum neutron wall load is about1.4 times of the average wall loading ;

✓The outboard neutron wall loading is about 20% higher than the Inboard wall loading;

✓ It should be considered for the variable of neutron wall loading distribution along radial direction.





Neutron Wall Loading Distribution along radial direction



One-Dimensional Shielding Analysis

Shielding requirement

It was assumed that the change ratio of coil electric resistance will not exceed 10%, neutron fluence of coil less than $1 \times 10^{19} n/cm^2$.

Shielding thickness

If the operation duty is 30%, and the neutron wall loading is $0.8MW/m^2$ and the thickness of shield is 40cm, CFETR can operate 20 years $_{\circ}$



Shielding thickness VS. Operating time



Simple 3-D Neutronics Analysis

Plasma parameter

parameter	unit	value
Major radius	m	5.3
Minor radius	m	1.2
Elongation	/	1.75
Triangularity Neutron wall loading	/ MW/m2	0.4 0.5



Calculation model

Blanket structure is same with 1-D model.

➤ Arrangement of In-B and out-B is same.

➤ 15 and 10cm scraping layer for IB and OB, respectively.

Space for divetor is taken in court.

Isotropic volume neutron source is used.



3-d analysis model



Tritium Breeding on IB and OB

- Based on calculation results of simple 3-D model, total tritium breeding rate (TBR) of the blanket is 1.26 (IB+OB)
- Results are normalized to 1 D-T fusion neutron.

About 70% of tritium breeding is contributed by outboard blanket, and 30% contribution from inboard blanket;
Max. contribution of tritium breeding rate occurs in 2nd ceramic breeder zone.

 Installing In-board tritium breeding blanket is necessary for Selfsufficiency.



Tritium breeding distribution



Power Density Distribution

On along radial direction

 If average neutron wall loading is 0.8MW/m², the total fusion power will be 350MW. Max. power density is 17MW/m3 which occur at first tritium breeding zone.





Power Density Distribution

On along Poloidal Direction

Poloidal power density distribution of FW, first tritium, beryllium and cooling plate zone.
 Power density of tritium zone is much higher than the other zones.





Schematic view of a layer poloidal slice of outboard blanket module

- Calculation model and Input data
- Dimensions, 443mm(Radial)X500mm(Toroidal)X10mm (Poloidal);
- > Including the FW of U-shape, breeding zones with 5 Li_4SiO_4 pebble beds and 4 Be pebble beds;
- Assumed to cool the FW and breeding zones independently;
- \succ Coolant is the helium of 8 MPa, and inlet temperature is 300 $^\circ$ C, outlet temperature is about 500 $^\circ$ C.



Preliminary thermal-hydraulic analysis



Analysis model and meshes



Global temperature distribution

Max. temperature for different materials

Materials	Max. Temp. [℃]	Allowable Temp. [℃]
First Wall RAFMs	522	550
Li_4SiO_4 pebble beds	613	920
Be pebble beds	554	650



Design Parameters of Solid Blanket

Neutron Wall Loading, NWL [MW/m ²]	0.4-0.8	
Tritium Breeding Ratio, TBR	1.26	
Coolant	He	
Inlet/Outlet Temperature, T [ºC]	300/500	
Pressure, P [MPa]	8	
Tritium Breeder (single size)	Li ₄ SiO ₄ Pebbles	
Li -6 Enrichment, %	80	
Filling ratio, %	60	
Max. Temperature, T [ºC]	613	
Neutron Multiplier (binary size)	Be pebbles	
Filling ratio, %	80	
Max. Temperature, T [ºC]	554	
Structure Material	RAFM	
Max. Temperature, T [ºC]	522	





Proposed CFETR blanket module concept



Critical Issue for Solid Breeder Blanket

- Critical issues associated with solid breeder materials relate to the following
- 1. Fabrication consideration of the ceramic breeder,
- 2. Property data base: chemical stability, physical properties, compatibility, residual activation.
- 3. Tritium release from solid breeder,
 - -- Temperature limits on breeder zone
 - -- Tritium breeding capability
- 4. Radiation effects on properties (swelling),
- 5. Thermal conductivity of Lithium ceramic breeder, complexity of cooling tube layout;
- 6. Neutron multiplication issues (beryllium pebble fabrication).
- 7. Tritium extraction, recovery, coolant purification and tritium permeation barrier technology.



Potential tritium breeding materials

	Li ₂ O	LiAlO ₂	Li ₂ ZrO ₃	Li ₄ SiO ₄	Li ₂ TiO ₃
Melting Point / K	1696	1883	1888	1523	1808
Density / g cm ⁻³	2.02	2.55	4.15	2.4	3.43
Li at. density / g cm ⁻³	0.94	0.27	0.38	0.51	0.43
Thermal conductivity (773 K) /W m ⁻¹ K ⁻¹	4.7	2.4	0.75	2.4	1.8
Reactivity with water	large	small	none	small	none
Tritium retention time (713 K) / h	8.0	50	1.1	7.0	2.0
Li Vaporization (in additional H_2)	> 600°C	> 900°C	> 800°C	> 700°C	> 800°C
Long period use (2 years)	Instability (Li vaporization)	Stability	Instability (crack)	Instability (Li vaporization)	Instability (Reduction of Ti)
Tritium release (easy release)	> 400°C	> 400°C	> 400°C	> 350°C	> 300°C
Optimum operating temp.	400 - 600°C	400 - 900°C	400 - 800°C	350 - 700°C	300 - 800°C
Tritium breeding ratio (TBR)	High	Lower	Middle	Middle	Middle

Li₄SiO₄ is considered as reference material and Li₂TiO₃ as alternative material for Chinese CFETR.



R&D Foundation for Solid Breeder Blanket

Structure Materials

- Two RAFM alloys have being developed in China; CLF-1 in SWIP and CLAM in ASIPP.
- Ton-class ingot of RAFM steel were recently produced



- Two kinds of ceramic breeders (Li₄SiO₄, Li₂TiO₃) are being developed at different institutions.
- Lithium orthosilicate (Li₄SiO₄) pebbles should be the primary option for FETR.

Neutron Multiplier

- Be metal of high performance has been developed in China.
- Be pebbles have been fabricated by Rotating Electrode Process (REP) method in China.

Test Facilities

 The construction of a small He Test Loop to validate circulator technology will be completed this year.





500kg Ingot of CLF-1

Mock-up of FW



Li₄SiO₄ Pebbles (D=1mm) by metl spraying method @SWIP



High flux Test Reactor



Sample of Be Pebbles(D=1mm)



REP Facility at HBSM Co.



Summary

 Based on mission and time schedule, the solid breeder blanket might be one of CFETR blanket options.

• TBR can achieve the tritium self-sufficiency (TBR >1.2) of based on current ceramic blanket model.

 Comprehensive consideration of breeding zone, shielding and vacuum chamber, the total thickness of blanket is not exceed 1.0 m.

 Preliminary thermal-hydraulic analysis shows that current blanket design parameters are feasible.



Thank you for your attention!