



An approach towards different design options for

DEMO:

Pulsed (conservative) versus steady-state (advanced) tokamak

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Development of 2 DEMO tokamak „working models“ for the German DEMO working group

- DEMO working models to serve as reference basis for the 13 sub-groups
- 2 tokamaks (pulsed vs. steady state) and 1 stellarator (see talk by C Beidler)
- Tokamak target requirements:
 - 1) „Conventional“ pulsed DEMO tokamak (conservative, low complexity)
 - *output power 1 GW_{el}*
 - accessing the economic parameter range for a power plant
 - *pulse duration many hours*
 - minimising impact of cyclic loads
 - *low or zero HCD level*
 - minimising recirculating power
 - minimising development needs for HCD system
 - *physics and technology as of today*
 - 2) „Advanced“ steady-state DEMO tokamak
 - *output power 1 GW_{el}*
 - *steady state via BS and HCD*
 - *moderate extrapolation in physics and technology*

Main elements:

- **Fusion power** calculated using the IBP98(y,2) confinement scaling

$$\tau_E / s = 0.173 H_H I_M^{0.93} R_0^{1.39} a^{0.58} \kappa^{0.78} n_{20}^{0.41} B_0^{0.15} P_M^{-0.69}$$

- **Pulse duration** (OH and non-inductive)
- **Heat + particle exhaust** model to adjust divertor power and core radiation
- simple **CoE estimation** $CoE \sim V_{tokamak} / P_{electr.}$

Benchmarking: Fair agreement with

- Model by H. Zohm
- DEMO PPPT 2011 benchmark case (D. Ward, J. Johner)
- European PPCS-A study (D. Maisonnier NF 2007)

In this analysis, **only the quantities marked in red are used as variables.**

- Different sets of these parameters are chosen for the pulsed + steady-state case

Input data		Output data
R_0 / m		
a / m		
$b = 1.8 m$		c / m
κ, δ		f_{shape}
$B_{max} = 13 T$		B_0 / T
q_{95}		I_p / MA
$N_{GW} = n/n_{GW}$		n_e
$H_H(IBM98 y,2)$		τ_E
$\tau_{\alpha}^* / \tau_E = 5$		C_{He}
$C_N = 0.01$		C_{Ar}
$C_W = 5 \times 10^{-5}$		Z_{eff}
(P_{ext} / MW)	(or)	(P_{ext} / MW)
$\eta_{therm} = 0.35$		P_{therm} / MW
$\eta_{HCD} = 0.4$		P_{electr} / MW
		P_{α} / MW
		P_{Div} / MW
		$P_{Core,rad} / MW$
		$T_e = T_i / keV$
		Q
		β_N, β_{pol}
		t_{pulse} / h
		$q_{Neutron} / MW/m^2$

Boundary conditions and assumptions

Plasma current:

$$q_{95} = 5 \frac{a^2 B_0}{I_M R_0} f \geq 3$$

(safety factor)

Plasma density:

$$N_{GW} \equiv \frac{n}{n_{GW}} = \frac{\pi a^2 n_{20}}{I_M} \leq 1.2$$

(Greenwald, Angioni)

Plasma pressure:

$$T_k \leq 0.39 \beta_{N,\max} \frac{B_0 a}{N_{GW}}$$

(beta limit)

Plasma shaping:

$$\kappa = 1.6 + 0.6 \frac{a}{R_0}; \quad \delta = \frac{\kappa - 1}{2}$$

(vertical stability)

Blanket thickness:

$$b = 1.8m$$

(distance separatrix – TF coil)

Magnetic field:

$$B_{\max} = 13T$$

(for TF coils and CS coil)

these determine B_0 :

$$B_0 = B_{\max} \left(1 - \frac{a+b}{R_0} \right)$$

(magnetic field at $R = R_0$)

TF radial build:

$$c = (a+b)/4$$

(after J. Freidberg)

Power balance:

$$P_{Heat} = P_{\alpha} + P_{ext} + P_{OH}$$

$$= P_{Sync} + P_{ImpRad,core} + P_{Rad,edge} + P_{Div}$$

$$P_{Sep} = P_{Rad,edge} + P_{Div}$$

$$> 1.3 P_{LH} \approx 2.2 n_{20}^{0.78} B_0^{0.77} a^{0.98} R_0^{1.00} \quad (\text{Y. R. Martin})$$

$$P_{Rad,edge} \approx P_{Mathews} - P_{ImpRad,core}$$

$$P_{Mathews} = 2.08 (Z_{eff} - 1)(1 + \kappa) a R_0 n_{20}^2 \quad (\text{Argon})$$

Assume that 2/3 of the divertor power is radiated:

$$P_{Div} \approx 3 \times 1.5 q_{max} F_x \lambda_q 2 \pi R_0 \quad (\text{D. Reiter, V. Kotov})$$

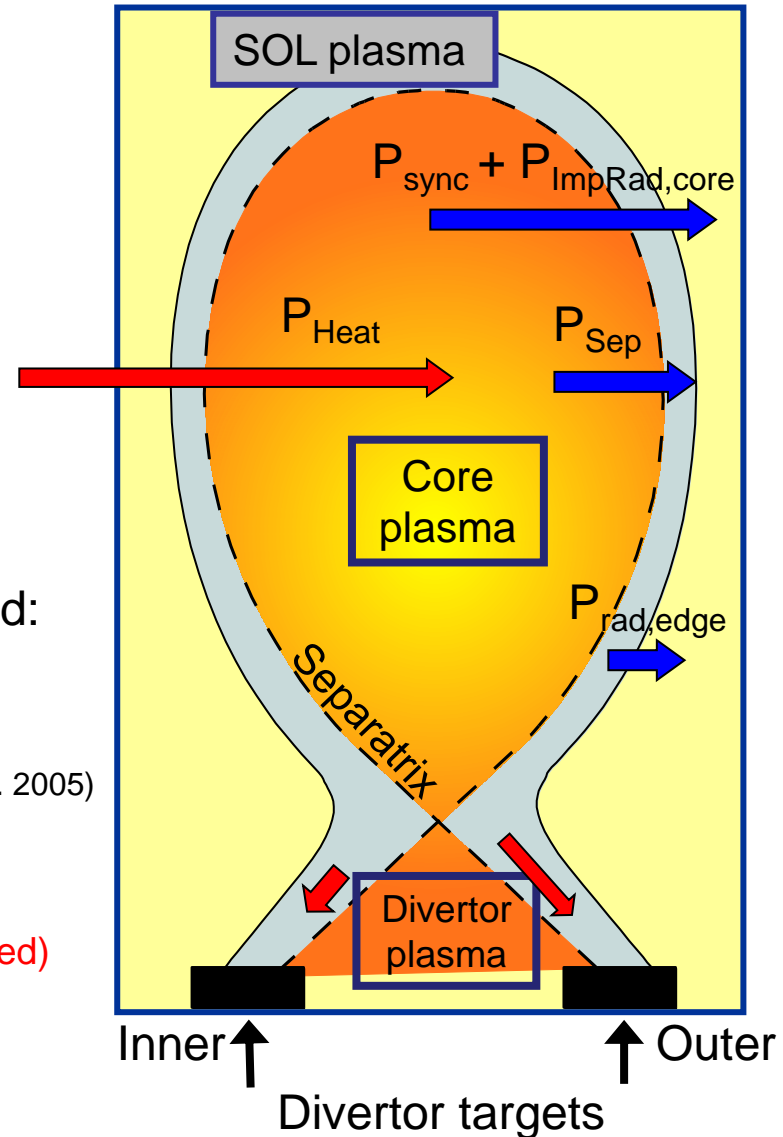
$$\lambda_q = 0.0008 \times R_0 \quad (\text{A. Kallenbach, J. Nucl. Mat. 2005})$$

$$F_x = 10$$

$$q_{max} = 5 \text{ MW} / \text{m}^2 \quad (q_{max} = 3 \text{ MW} / \text{m}^2 \text{ preferred})$$

Particle exhaust:

$$\frac{\tau_{\alpha}^*}{\tau_E} = 5$$



Pulse duration:

$$t_{Pulse} \approx \frac{\Phi_{CS} + \Phi_{BV} - \Phi_{ignition} - (\epsilon_{ejima} \mu_0 R_0 + L_{plasma}) I_{Plasma}}{R_{Plasma} I_{Plasma} (1 - f_{BS} - f_{CD})}$$

Bootstrap current:

$$f_{BS} = 0.7 \sqrt{\frac{1}{A}} \beta_{pol}$$

Current drive:

$$\frac{I_{CD} [MA]}{P_{Ext} [MW]} = \gamma_{CD}(T) \cdot \frac{1}{n_{20} \cdot R_0}$$

using

$$\gamma_{CD}(T) = 0.4 \frac{T / keV}{15}$$

and

$$\eta_{CD} = 0.4$$

(aiming for ECRH)

Plant power balance:

$$P_{el} = \eta_{th} (1.18 P_{Fus} + P_{HCD} + P_{OH})$$

using

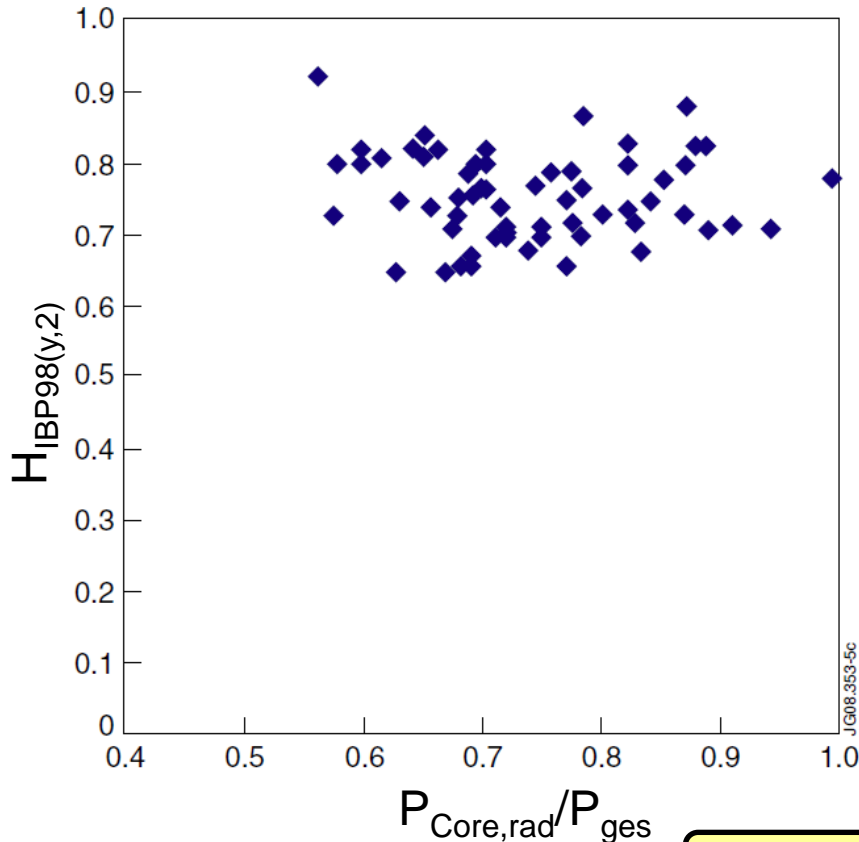
$$\eta_{th} = 0.35$$

(conservative, leaving room for He cooling power)

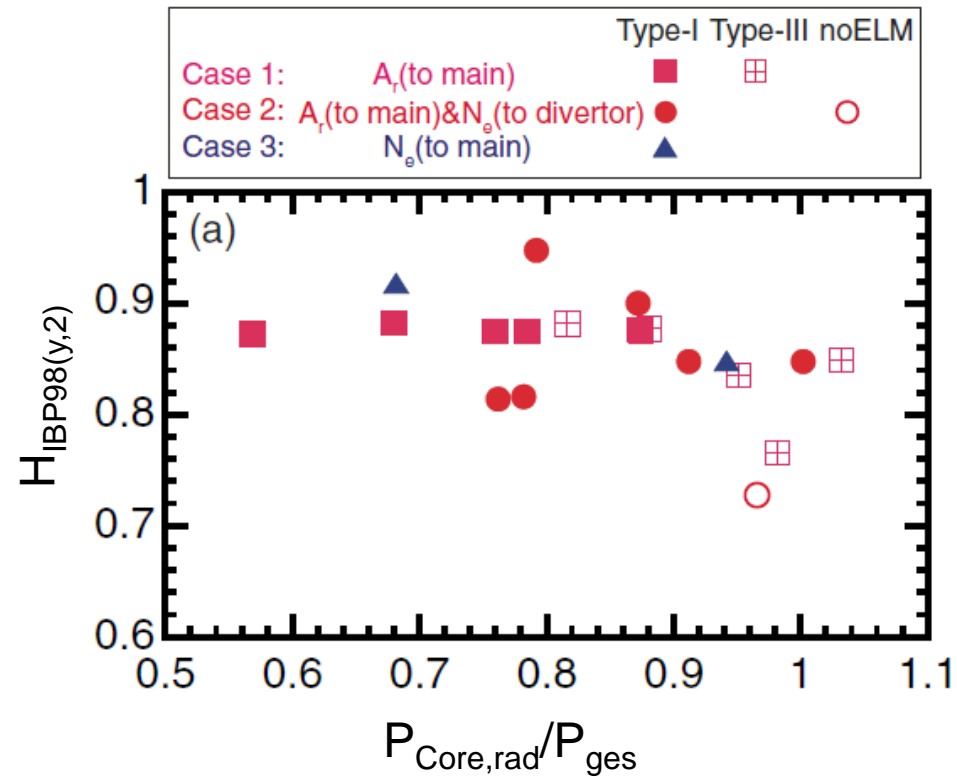
Radiative H mode: Plasma scenario for the „conservative“ pulsed DEMO tokamak

Experimental results from JET and JT-60-U:

JET (J. Rapp Nucl. Fusion 2009)



JT-60U (N. Asakura Nucl. Fusion 2009)



Summary of results:

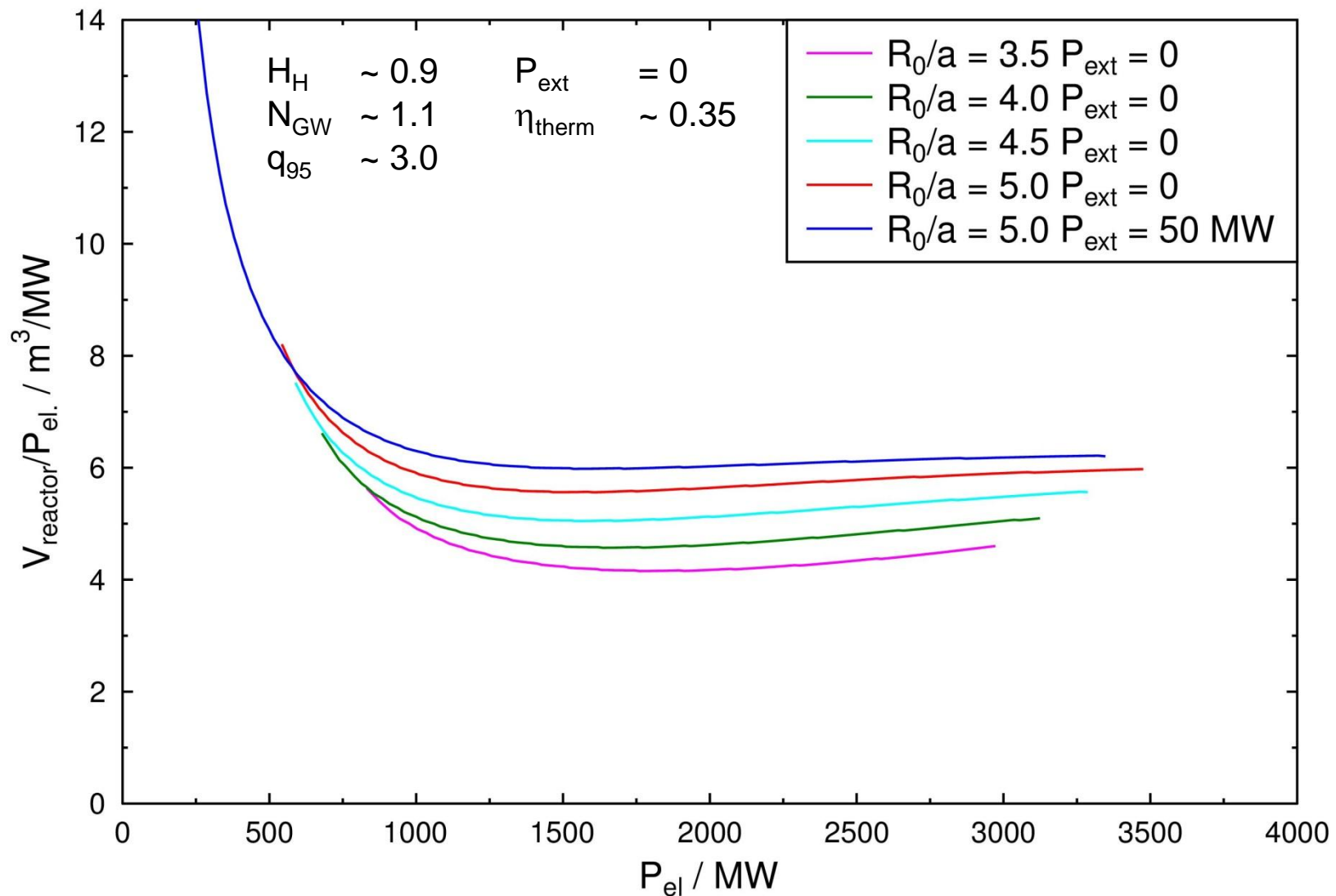
taking into account radiation explicitly $\rightarrow H_H = 0.9$

- consistent parameter set $H_H = 0.85$ with $N_{GW} = 1.0$ and $P_{core,rad}/P_{ges} = 0.6 \dots 0.9$
- ELM size strongly reduced (Type III ELMs)

Pulsed tokamak: „Cost of Electricity (CoE)“

0-dimensional tokamak fusion reactor model

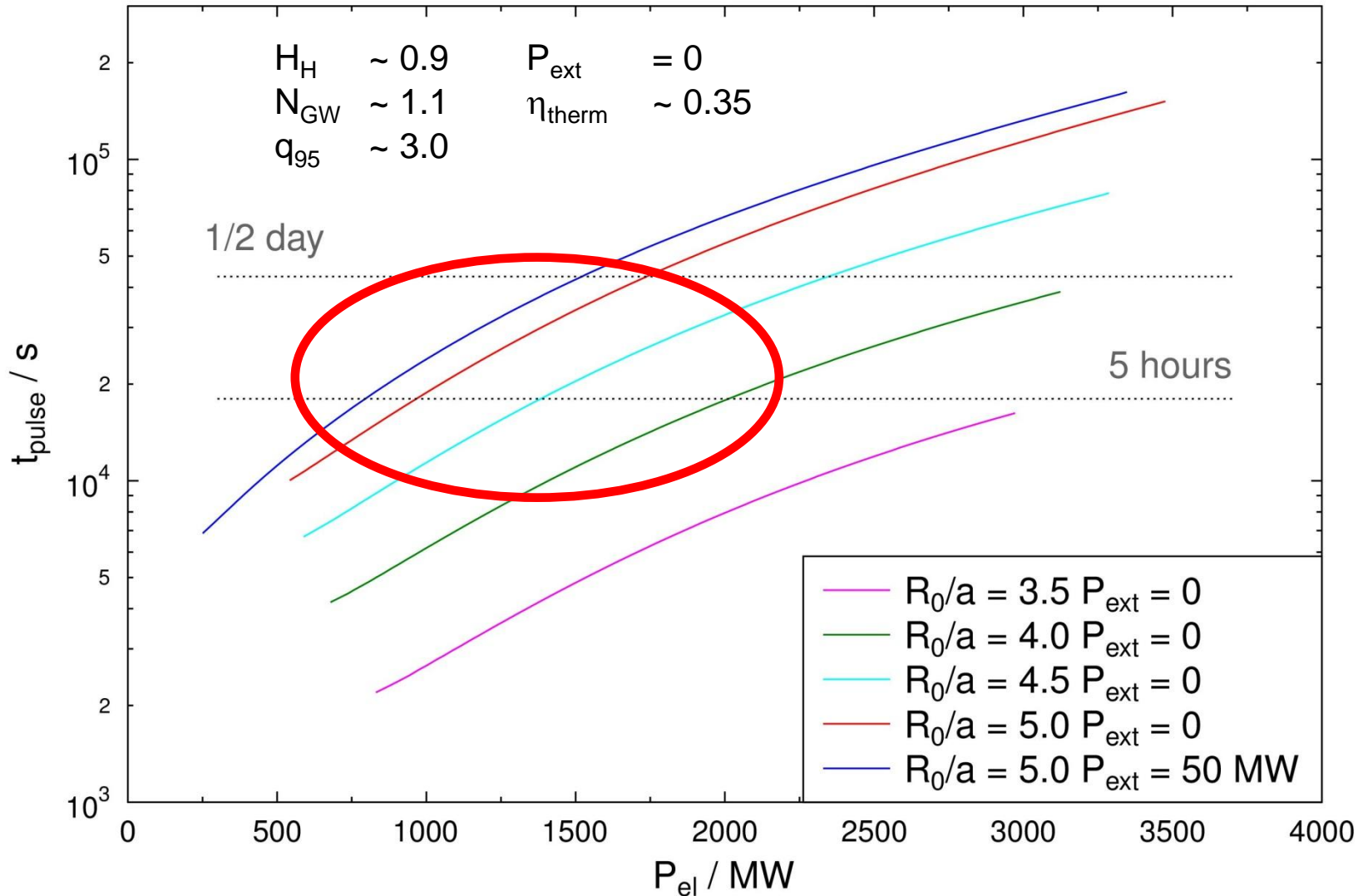
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Pulsed tokamak: Plasma pulse duration

0-dimensional tokamak fusion reactor model

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Parameter range for pulsed tokamak DEMO model ($P_{el} = 1 \text{ GW}$, $R_0/a = 5$, $\kappa = 1.72$, $\delta = 0.36$, $P_{ext} = 0$)

H_H	n/n_{GW}	q_{95}	a / m	R_0 / m	CoE	$q_{\text{neutron}} / \text{MW/m}^2$	$P_{\text{RadCore}}/P_{\text{Heat}}$	$T_{\text{pulse}} / \text{h}$
0.9	1.1	3.0	2.25	11.25	5.9	1.87	0.56	5.3
0.85	1.0	3.2	2.62	13.10	8.1	1.38	0.56	9.0

Approach for pulsed tokamak DEMO

- choose large aspect ratio to allow for large CS coil and long pulse duration
- operate near the maximum possible n/n_{GW} and plasma current (low q_{95})
- External heating essential only for start-up

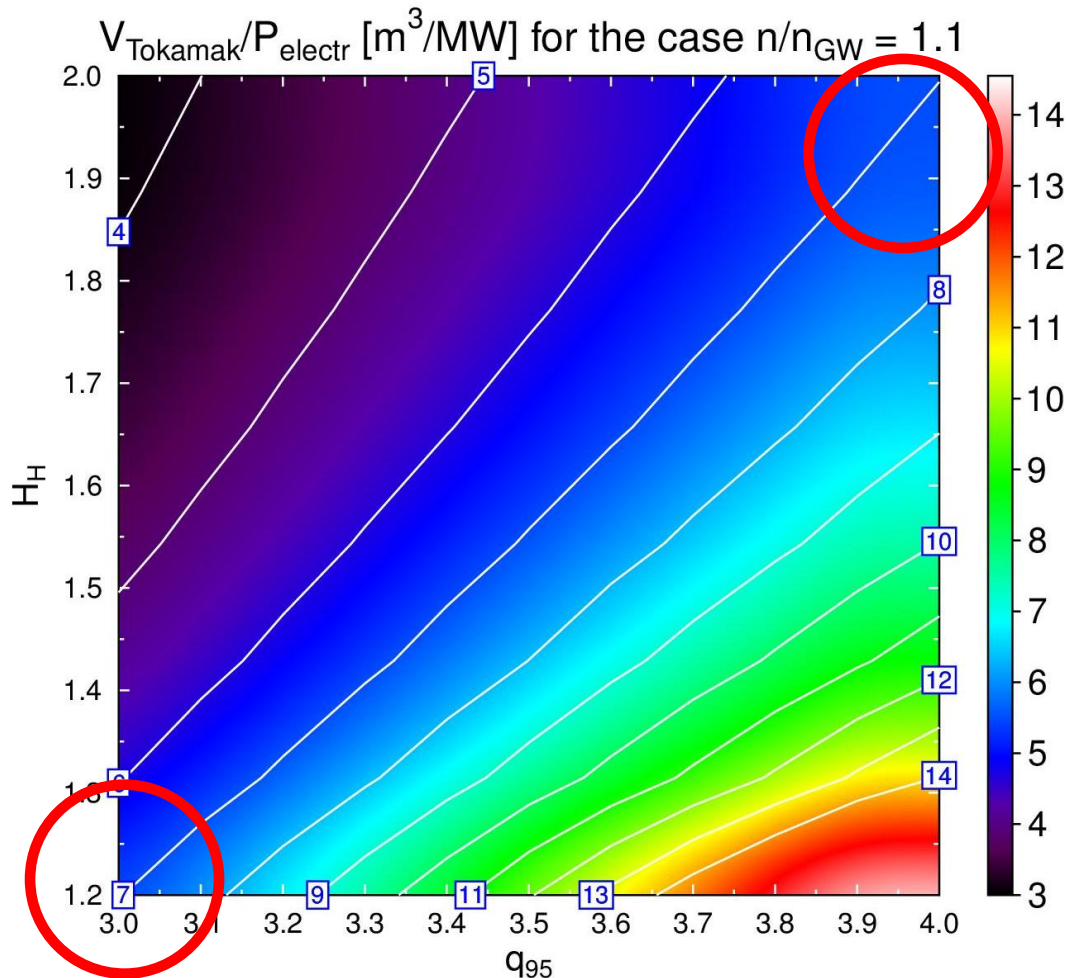
Main properties

- minor radius $a \sim 2.2 \text{ m} \dots 2.6 \text{ m}$, **10% .. 30% larger than ITER**
- pulse duration several hours, inductive drive
- moderate plasma core radiation, $q_{\text{max}} = 5 \text{ MW/m}^2$

Steady state tokamak solutions:

$N_{GW} = 1.1$, $P_{electr,net} = 1$ GW, $R_0/a = 3$, $\kappa = 1.8$, $\delta = 0.4$

$$CoE \sim V_{tokamak} / P_{electr,net}$$



2 different possible approaches with comparable performance:

- Advanced scenario with $q_{95} = 4$ ($q(r) > 2$ everywhere) and very high confinement ($H_H > 1.6$)
- Standard H mode with $q_{95} = 3$ and somewhat improved confinement ($H_H = 1.2$)

Parameter range for steady-state tokamak DEMO model ($P_{eI} = 1 \text{ GW}$, $R_0/a = 3$, $\kappa = 1.8$, $\delta = 0.4$)

H_H	n/n_{GW}	q_{95}	a / m	R_0 / m	CoE	$q_{neutron} / MW/m^2$	$P_{RadCore}/P_{Heat}$	T_{pulse} / h
1.6	1.2	4.0	3.2	9.6	7.1	2.3	0.70	∞
1.2	1.1	3.0	3.16	9.5	6.9	3.07	0.68	∞

Optimisation strategy for steady-state tokamak

- Two different routes:
 - either **advanced tokamak** with $q_{95} = 4$ ($q > 2$ everywhere) and very high confinement factor H_H (**preferable due to lower HCD power needed**)
 - otherwise more **conventional H mode** tokamak with $q_{95} = 3$ and confinement-optimisation ($H_H = 1.2$) similar to the PPCS model A / AB

Main properties

- minor radius $a > 3 \text{ m}$, **> 50% larger than ITER**
- full steady-state operation, current drive with $P_{HCD} > 200 \text{ MW}$
- high plasma core radiation, $q_{max} = 5 \text{ MW/m}^2$

Issue	Pulsed	Steady-state
H_H / q_{95}	0.9 / 3.0	1.6 / 4.0
CoE (rel. units)	1	1.2 + cw HCD system
FW lifetime (75dpa) / y	4.0	3.2
C_{Ar}	0.3%	1.0% (→ FW sputtering)
Need for HCD	Start-up + control	> 200 MW steady-state
Need for profile control	No	Yes
Load cycling	Medium	low

Issues for further elaboration:

- Plasma scenario
- First wall lifetime
- Disruptions
- Plasma control
- Plant availability

Pulsed tokamak with large aspect ratio R_0/a and radiative H mode

- plasma scenario with **high radiation fraction, high density and small ELMs** exists
 - *needs further optimisation and testing on ITER, JT60SA, ...*
- possible issue with LH threshold (?), ELM size may be still too large (?)
- parameters are not fully compatible with settings chosen for the IBP98(y,2) database
 - *develop new database and scaling law for radiative H mode*
 - *clarify density scaling, beta scaling, radiation scaling, ...*

Steady-state tokamak with advanced scenario / improved H mode

- real steady-state performance still to be demonstrated
 - *experiments on ITER, JT60SA, ...*
 - Required HCD level, radiation level and confinement scaling to be explored
 - *optimisation needed to make this approach attractive*
 - Scenario depends on feasibility of economic current drive and control systems
- **DEMO physics basis to be developed**

Issues (2): First wall lifetime (P3, T2, T3 working groups)

Issue	Pulsed	Steady-state
H_H / q_{95}	0.9 / 3.0	1.6 / 4.0
FW lifetime (75dpa) / y	4.0	3.2
C_{Ar}	0.3%	1.0% (→ FW sputtering)

Limitation of power flux density to the target plates ($q_{\max} = 5 \text{ MW/m}^2$) via radiation

→ enhanced (core and edge) radiation

→ limitation of $P_{\text{sep}} = P_{\text{Heat}} - P_{\text{RadCore}}$

→ moderate power density (→ larger machine volume for a given P_{el})

First wall sputtering: ~ main chamber 0.1 mm / y (Brooks), in divertor probably more

Observations:

- For the case of a „traditional divertor“, the pulsed tokamak with radiative H mode may have lower neutron damage rate, lower sputtering by impurities
- **In comparison, the steady-state tokamak seems less attractive unless there would be a different approach for power handling**
- However, load cycling issues to be quantified

Energy released in a disruption on DEMO

(assuming operation near density limit and beta limit):

- Current quench: $W_{\text{ind}} \sim a^3 B^2 / A q_{95}^2 \sim 1 \text{ GJ}$ (several 10 ms)
- Thermal quench: $W_{\text{th}} \sim a^3 B^2 / q_{95} \sim 1 \text{ GJ}$ (a few ms)

An **unmitigated disruption** would release the stored energy W_{th} to the divertor plates → **factor 30 .. 100 about damage threshold** (M. Lehnen)

Disruption mitigation aiming at uniform spread of thermal energy via core radiation

- Since $S_{\text{Wall}} \sim 1500 \text{ .. } 3000 \text{ m}^2$, the mean energy density is $\sim 0.5 \text{ MJ/m}^2$

High risk of wall damage for each disruption with non-uniform energy release

Since $W/S \sim a$, the damage risk increases with machine dimensions

Diagnostics and actuators on a fusion reactor will be quite limited

- limited access and performance (large coverage of breeding blanket needed)
- limited lifetime (diagnostic+control components mainly behind the blanket)

Pulsed tokamak with large aspect ratio R_0/a and radiative H mode

- control of global / averaged plasma quantities:
 - q_{95} , $\langle n \rangle / n_{GW}$, β , P_{rad} , P_{fus} , ...
- plasma position and shape, heat fluxes, wall temperatures
- instabilities (disruption avoidance/mitigation)

Steady-state tokamak with / advanced scenario

- additionally control of local plasma quantities / plasma profiles is needed:
 - $n(r)$, $T(r)$, $j(r)$, ...
- **Feasibility of control system may limit the achievable complexity of the DEMO plasma scenario**

5 different types of downtimes / load variations to be distinguished

- Large shutdown for 1st wall replacement (intervals 3-4 y)
- Scheduled maintenance (e.g. removal of dust or stored tritium)
- unscheduled maintenance (repair of damage)
- power variations requested due to economic reasons (off-peak periods)
- **break between 2 pulses (only pulsed tokamak)**

Pulsed tokamak ($A = 5$): **Estimation of dwell time** between 2 pulses

- plasma termination (current ramp-down) ~ a few minutes
- Re-charging of CS coil ($r_{CS} = 6 \dots 7 \text{ m}$) ~ 20 .. 30 min ($P = 100 \text{ MW}$)
- Pump-down time estimated to ~ 20 min (C. Day)
- plasma startup ~ a few minutes
- thermal time constant of 1st wall ~ several minutes
- **minimum total break between 2 pulses ~ 1 hour**
- AC operation under consideration (2 divertors)
- coverage of break by thermal storage to be considered

- 2 DEMO tokamak working models ($P_{el} = 1$ GW) are being discussed in the German DEMO WG
 - Pulsed large aspect ratio tokamak ($t_{pulse} \sim$ several hours)
 - steady-state (advanced) tokamak ($P_{HCD} > 200$ MW)
- Main issues:
 - plasma scenarios to be further developed (\rightarrow „DEMO physics basis“)
 - 1st wall lifetime
 - *limited by sputtering and neutron embrittlement (< a few years)*
 - Disruptions
 - *are an essential problem for any DEMO tokamak*
 - plasma control likely to be a critical issue, in particular for
 - *disruption avoidance*
 - *1st wall protection*
 - *profile control*
 - Availability
 - *not too different for both DEMO tokamak models, if load cycling is not a problem*