



Divertor Design Considerations for CFETR

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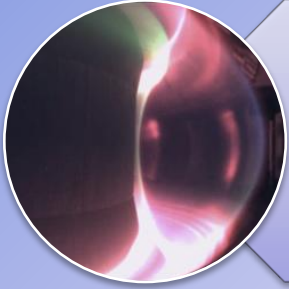
Houyang Guo

and Institute of Plasma Physics, Chinese Academy of Sciences

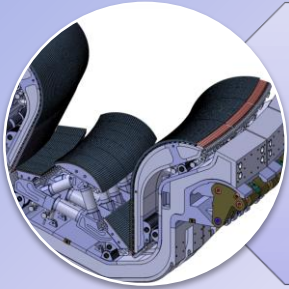
2nd International Workshop on CFETR

May 30 – June 1, Hefei, China

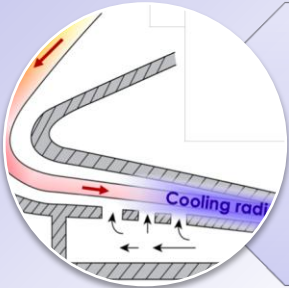
OUTLINE



**Key PSI issues for
CFETR**

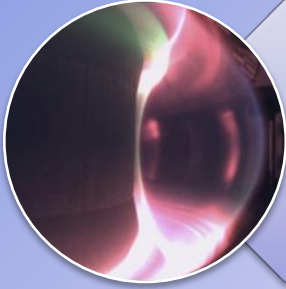


**CFETR Divertor
options**

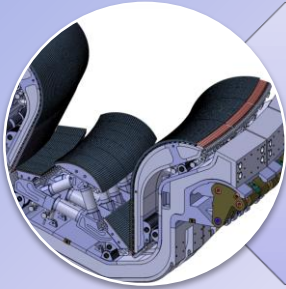


**Alternative target
concepts**

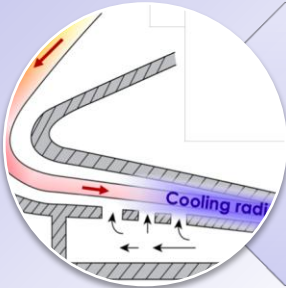
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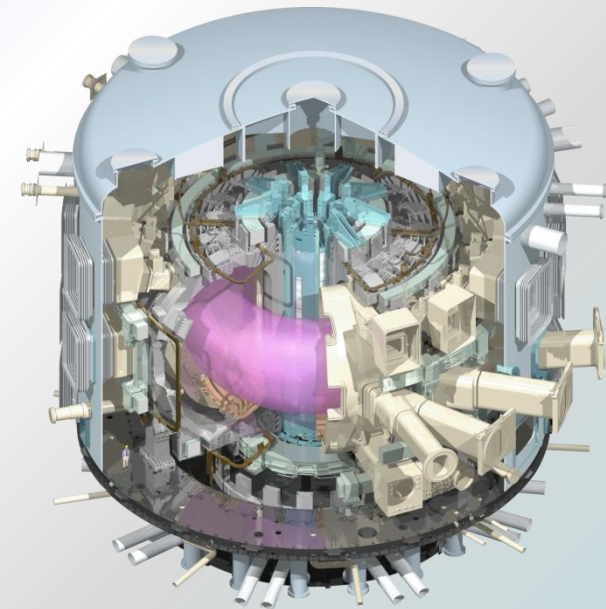
**CFETR Divertor
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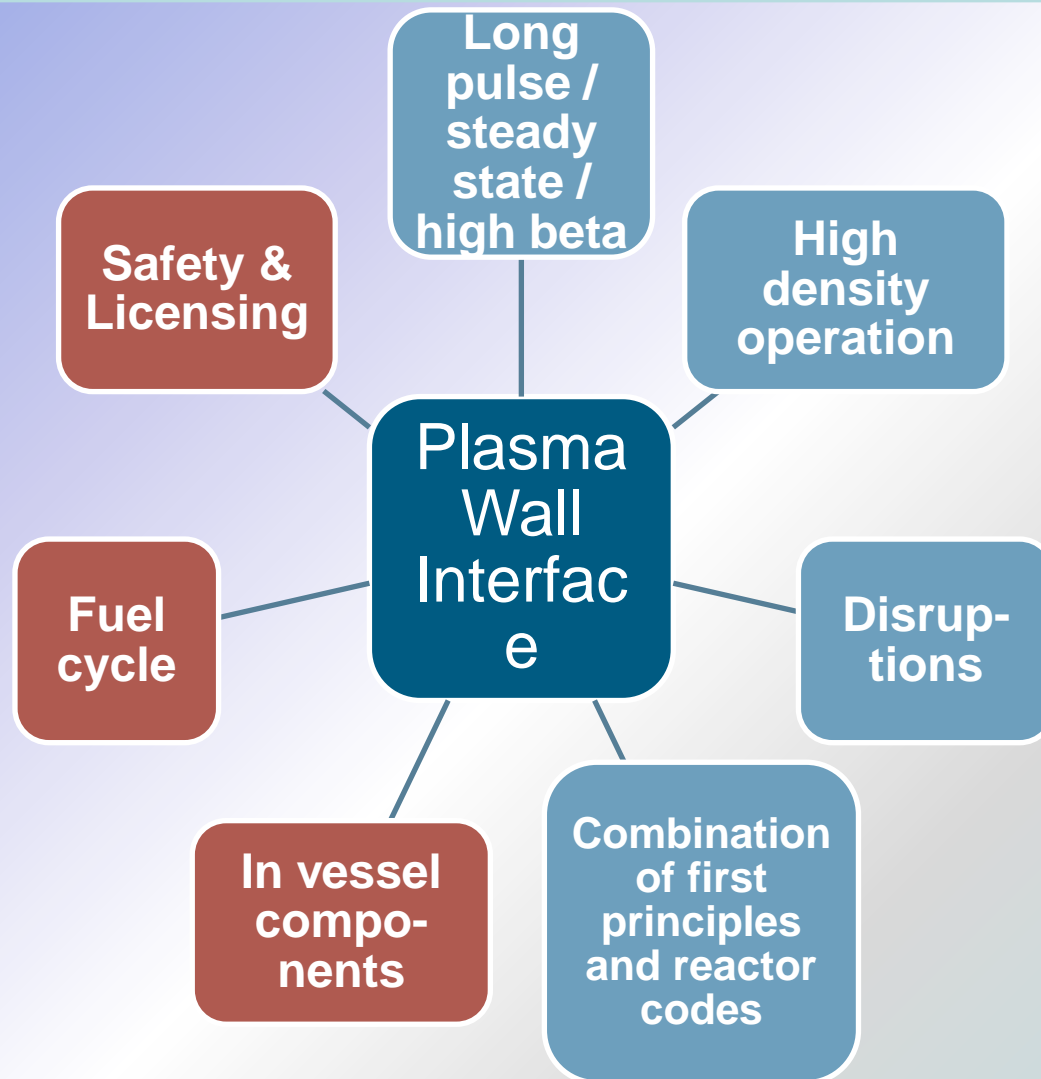
**Alternative target
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CFETR-main parameters (CFETR-00-00-03)

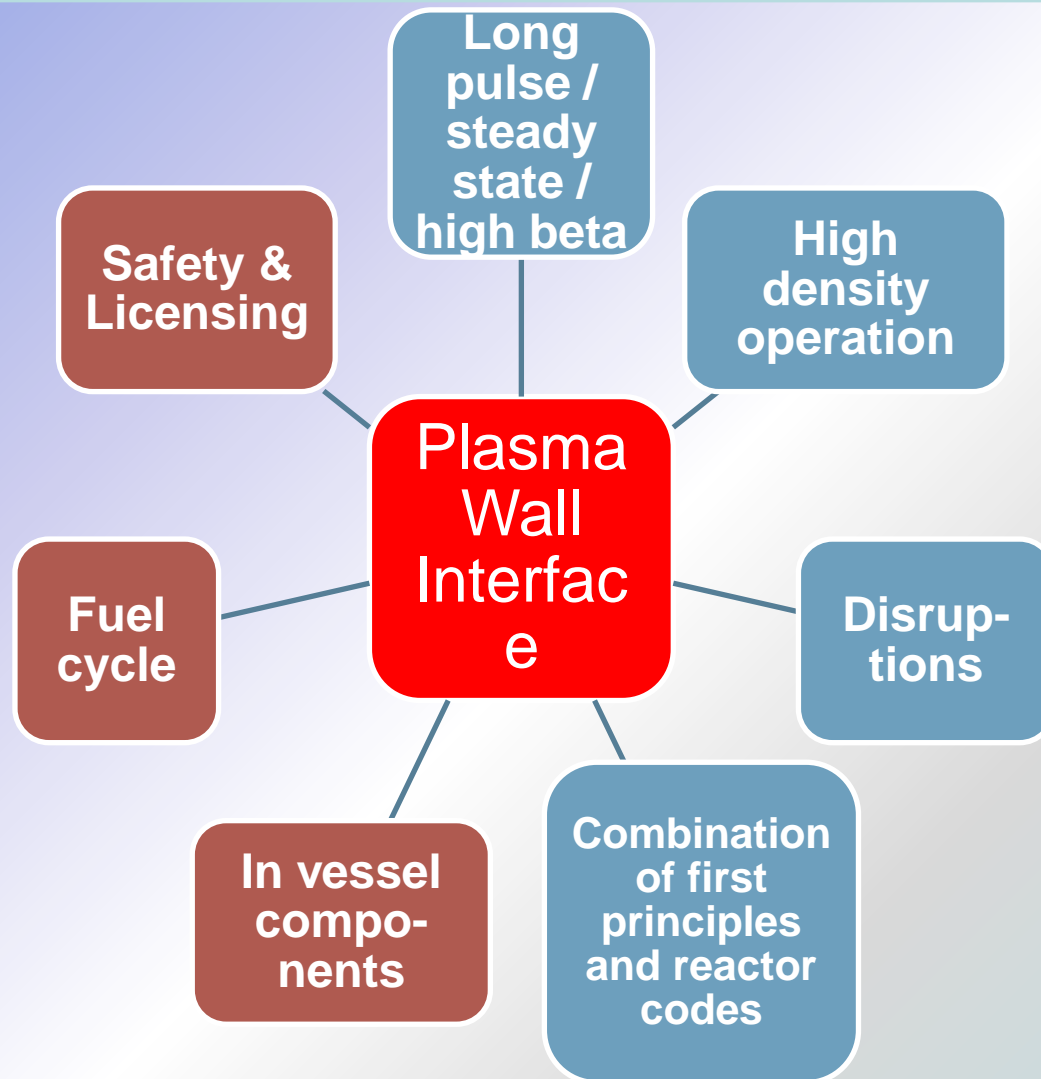
	CFETR	ITER
Major radius (m)	5.5	6.2
Minor radius (m)	1.6	2.0
Elongation	1.8	1.85
Plasma current (MA)	12/10/7	15 (17)
Toroidal field (T)	5.3/4.5	5.3
Central density ($10^{20}/\text{m}^3$)	(1.0)	1.0
Central temperature (keV)	(15)	20
Confinement time (s)	(1.5)	3.7
Heating Power (MW)	50/80	73
Fusion power (MW)	50~200	500 (700)
Plasma volume (m^3)	500	830
Operation time (s/ yr)	$1-1.6 \cdot 10^7$	$4.0 \cdot 10^5$



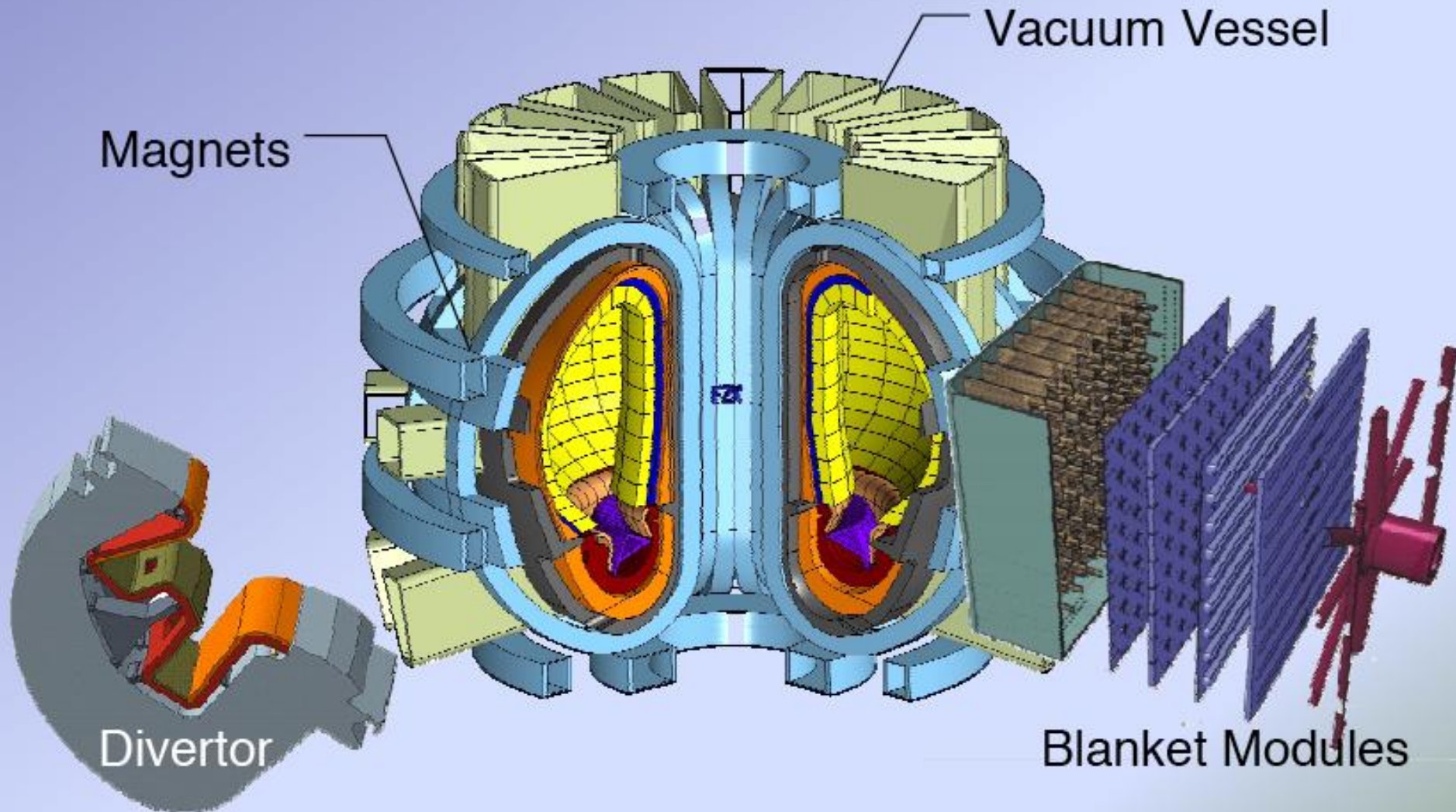
Integral Approach Is Mandatory for the Design of Plasma-Wall Interface



Integral Approach Is Mandatory for the Design of Plasma-Wall Interface



Divertor Is a Key Component for CFETR



Main Challenges for Divertor

- Exhaust the major part of the plasma thermal power, reducing heat flux below limitation of target materials.
- **Remove** fusion helium ash from core plasma while providing sufficient **screening** for impurities from wall.
- Maintain acceptable erosion rate in terms of reactor lifetime.

Selection of High Heat Flux Materials for DEMO Divertor Target

B. Unterberg, 20th PSI Conf. 2012, Germany

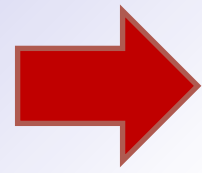
**Melting Point >2000 K
Thermal Conductivity >50 W/mK**

24 Cr Chromium 2180		6 C Carbon 3823	
41 Nb Niobium 2750	42 Mo Molybden... 2896	43 Tc Technetium 2430	44 Ru Ruthenium 2807
45 Rh Rhodium 2237	73 Ta Tantalum 3290	74 W Tungsten 3695	75 Re Rhenium 3459
76 Os Osmium 3306	77 Ir Iridium 2739	78 Pt Platinum 2041.4	

+

**Availability,
Cost**

24 Cr Chromium 2180	6 C Carbon 3823
41 Nb Niobium 2750	42 Mo Molybden... 2896
	74 W Tungsten 3695



+

**Low/Medium
Activation**

24 Cr Chromium 2180	6 C Carbon 3823
74 W Tungsten 3695	

+

Irradiation

24 Cr Chromium 2180	74 W Tungsten 3695
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+

e.g. T_{RC}

74 W Tungsten 3695

Major Problem for W is Melting under Transient Heat Load

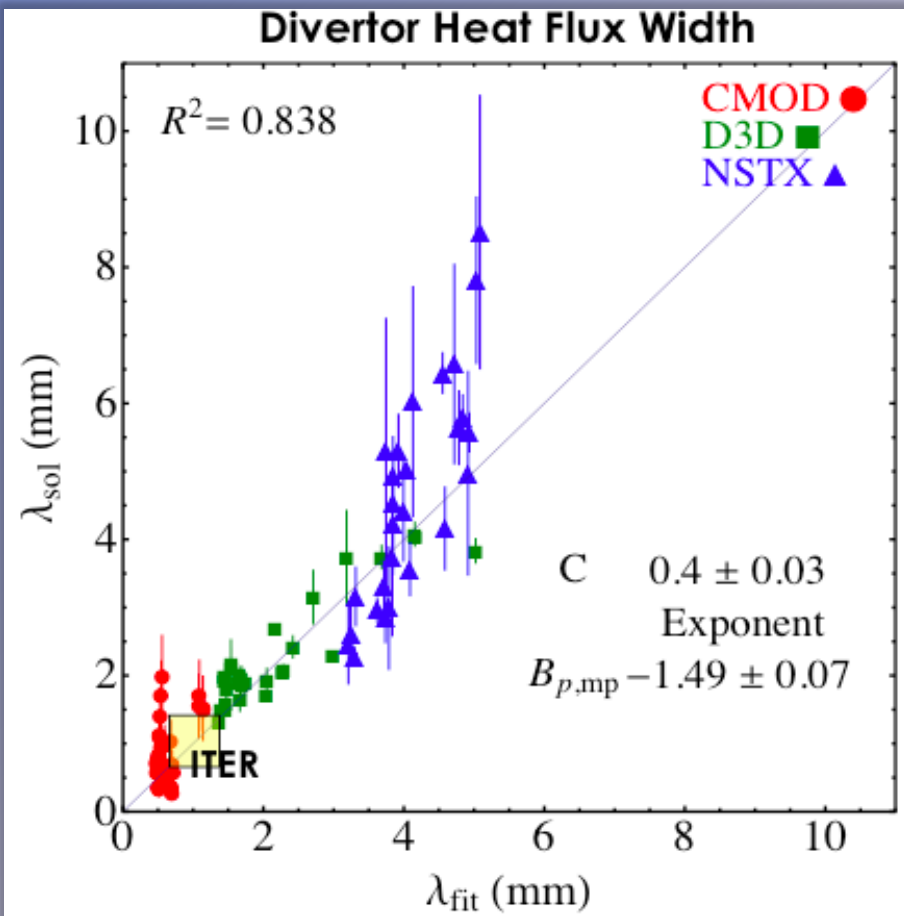
R. Haange, ITER STAC-12,/2012, Cadarache

W melting parameter: $\epsilon_{\text{melt}} \geq 50 \text{ MJm}^{-2}\text{s}^{-1/2}$

I_p (MA)	P_{IN} (MW)	Stored energy (MJ)	$E_{\text{transient}}$ (MJ)	$\lambda_{q\parallel\text{omp}}$ (m)	q_{target} (MJ m ⁻²)	ϵ (MJ m ⁻² s ^{-1/2})	Type
7.5	40	75	25 → 38	0.01	0.83 → 8.3	15.2 → 213	Disruption
15	50	350	88 → 175	0.005	5.78 → 76.9	105 → 1984	Disruption
7.5	40	75	6.4 → 8.0	0.01	1.39 → 1.74	77 → 123	Type I ELM

- Disruptions and unmitigated ELMs are predicted to melt W target for ITER (above).
- This will also apply to CFTR → **Disruption & ELM mitigation are mandatory.**
- **W Melting detection and RH are required to repair W damage.**

SS Heat Exhaust Is Also Challenging due to Very Narrow Power Deposition Width



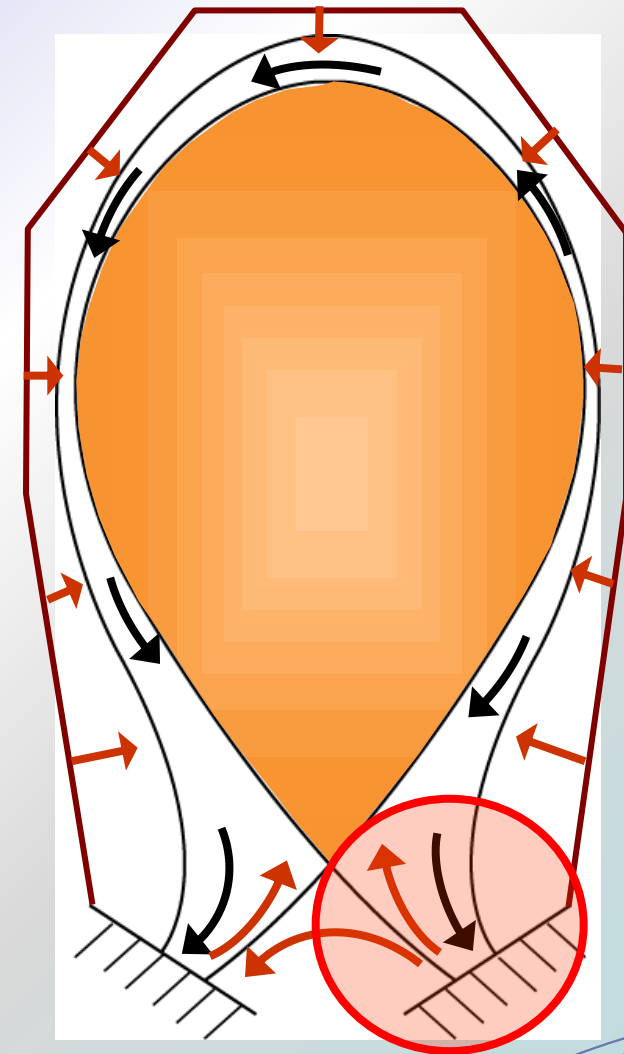
Detachment is required.

CFETR Faces Much Greater Challenges than ITER due to Larger Duty Cycle $\geq 0.3 \sim 0.5$

General migration pattern seen in today's devices: main wall erosion, convection into divertor \rightarrow deposition

R. Pitts, 2012 KSTAR Meeting

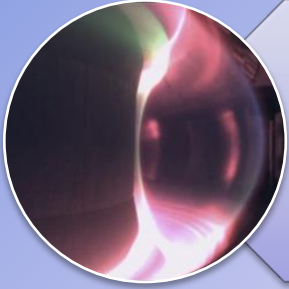
	No. Pulses (Y2000-2008)	Time in diverted Phase (hr)	Outer divertor ion fluence
JET	13466	40.5	$\sim 5 \times 10^{27}$
ITER	1	0.15	$\sim 1.5 \times 10^{27}$



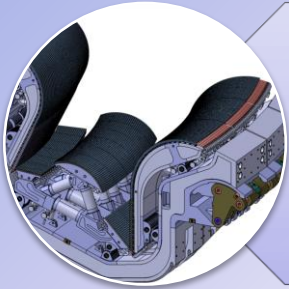
\rightarrow 9 years JET operation \sim 3 ITER $Q_{DT} = 10$ pulses in terms of divertor fluence, important for target erosion and T-retention

\rightarrow Much more serious for CFETR

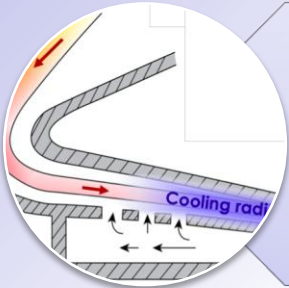
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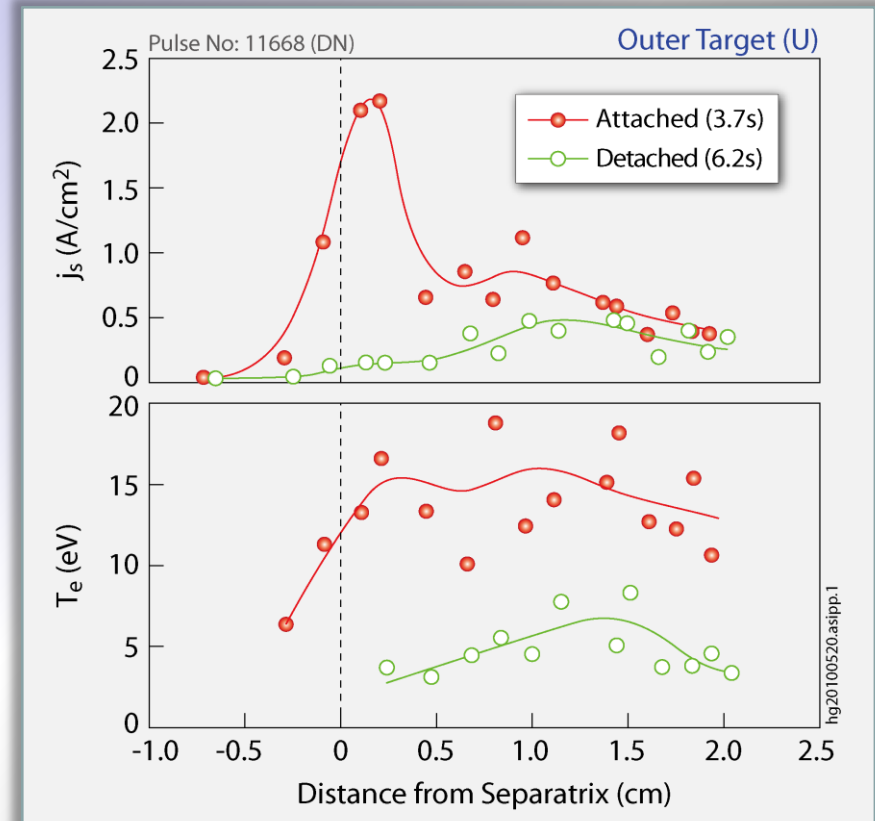
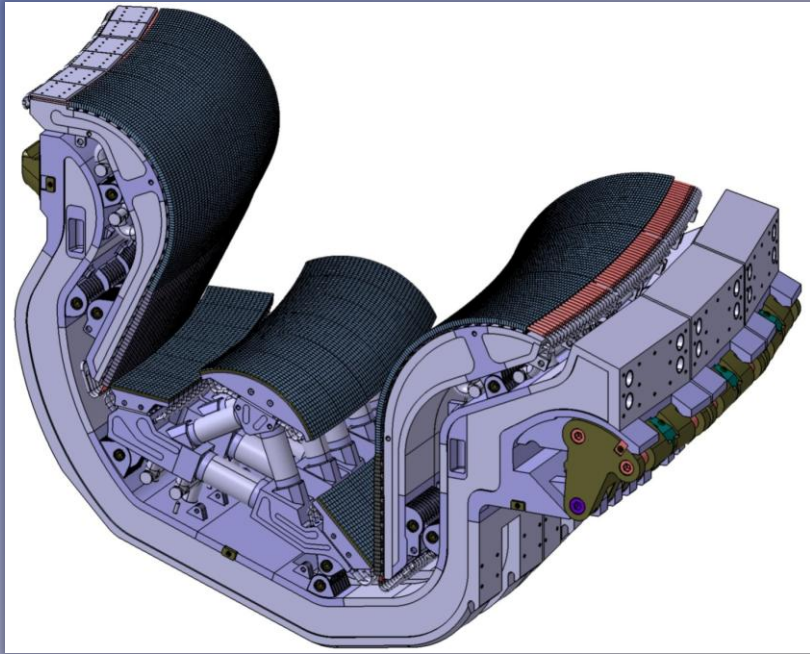


**CFETR Divertor
options**



**Alternative target
concepts**

ITER-Like Vertical Target Structure



- Promote detachment near strike point due to preferential ionization near strike points.
- Provide sufficient He ash removal.

System Design & Integration

- **Divertor cassettes with plasma facing components**
- **Cooling system to exhaust plasma and neutronic heat deposition**
- **Cryopumps to exhaust neutralized gas**
- **Fuelling system to promote plasma detachment / mitigate re-attachment**
- **Divertor view system and RH to monitor and repair divertor components...**

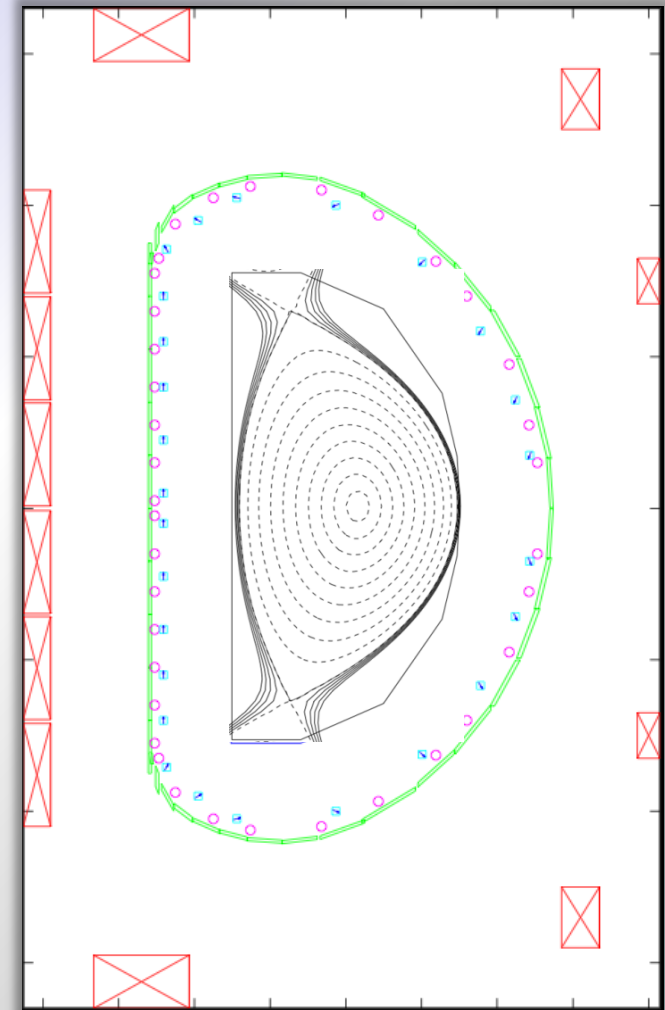
SD or DN ?

Advantages of DN:

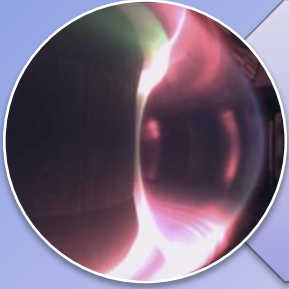
- Larger plasma-wetted area, facilitating power exhaust
- Allowing pumping via both top and bottom, facilitating particle exhaust
- Naturally large triangularity, facilitating advanced tokamak operation
- Accommodate Advanced divertor configuration, e.g., SXD

Advantages of SN:

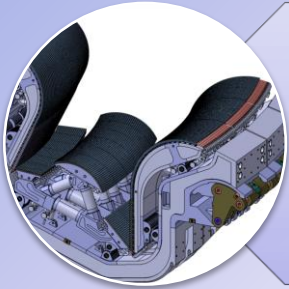
- Accommodating large plasma volume
- Maximizing TBR



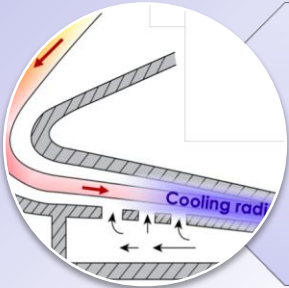
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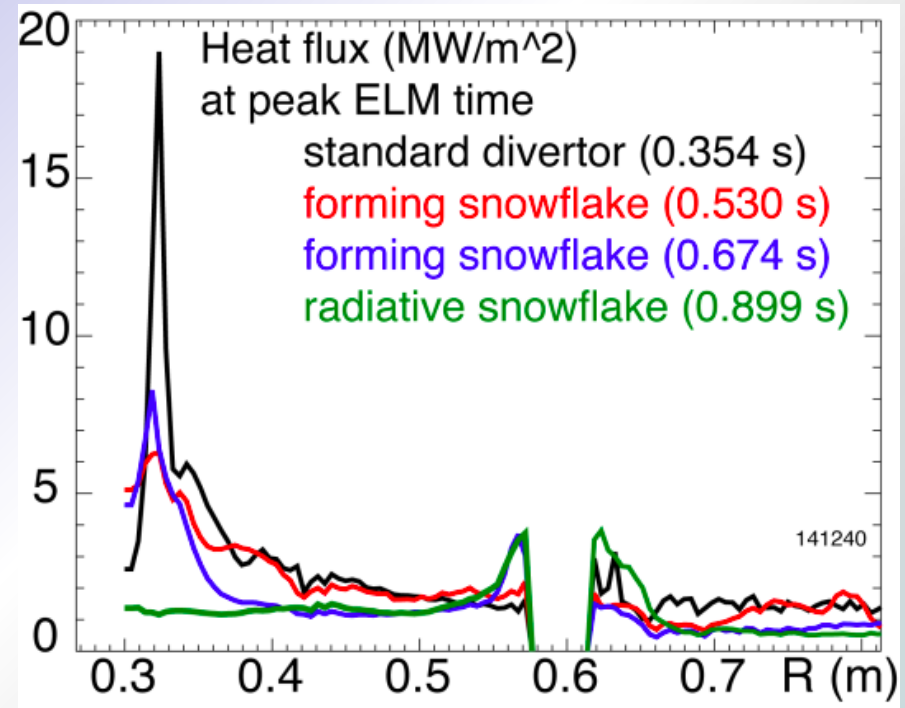
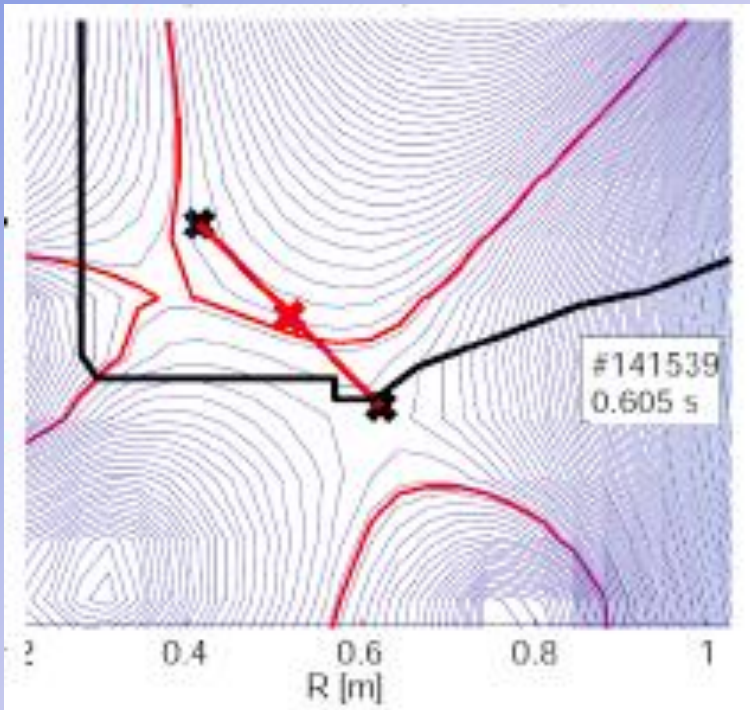


**Alternative target
concepts**

Snow-Fake Divertor to Reduce Peak Heat Load

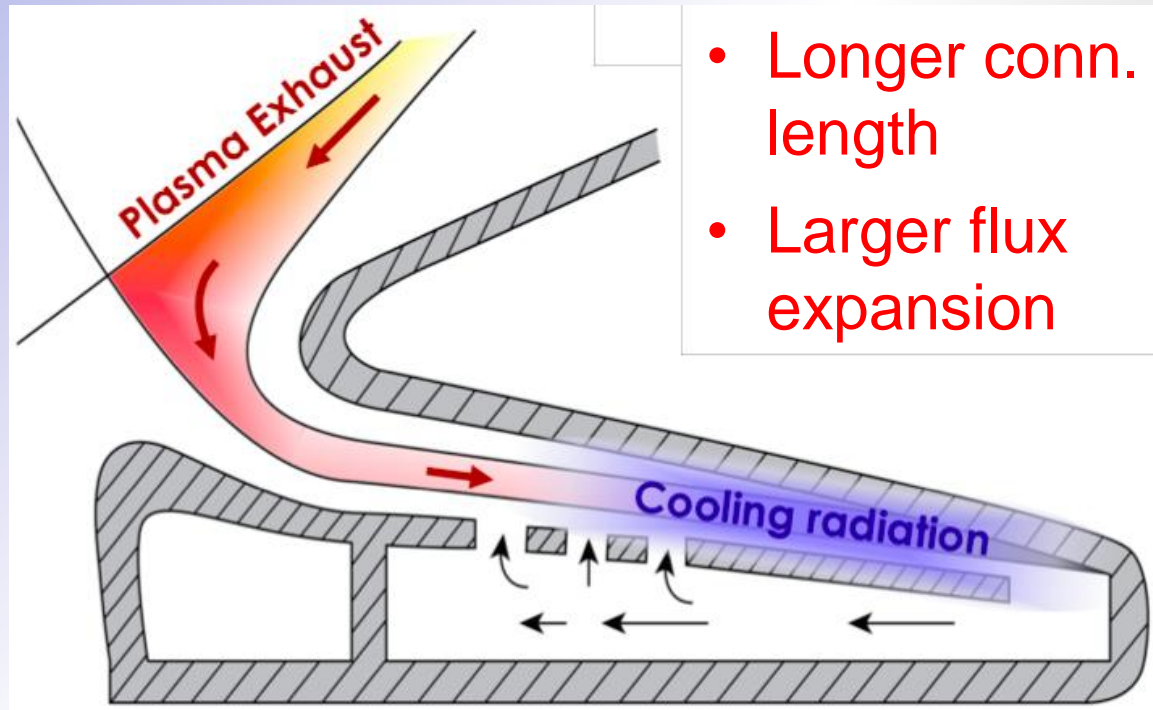
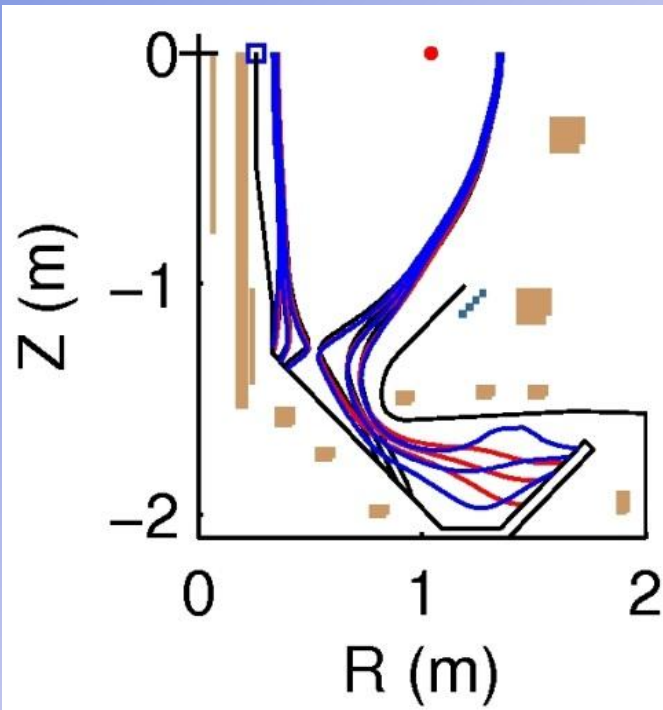
NSTX Snowflake Divertor

V.A. Soukhanovskii, NSTX-PAC 31, PPPL, April 17-19, 2012



- Reduction from 3-7 MW/m² to 0.5-1 MW/m² between ELMs;
Reduction from ~20 MW/m² to 2-8 MW/m² at ELM peak.

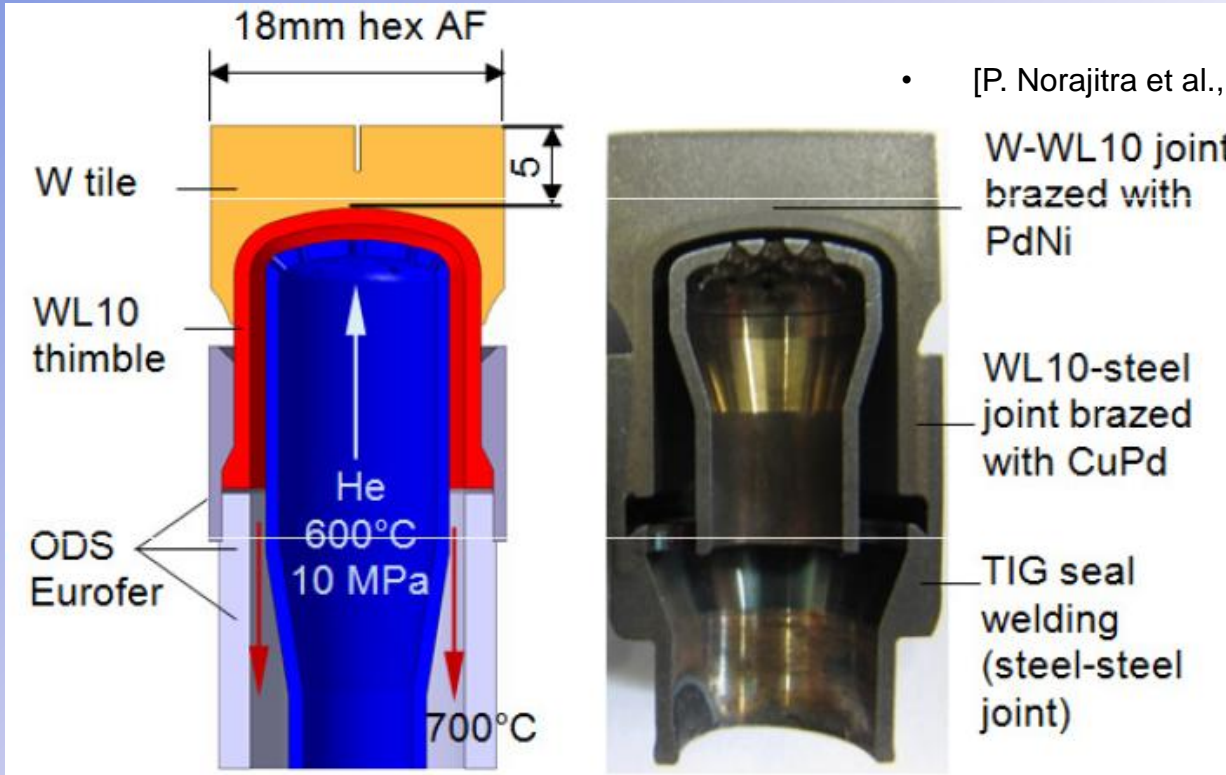
Super-X / Isolated Diverter



Critical issue:

DEMO compatible coils to establish configuration

High Temperature Operation



**He-cooled modular divertor
with jet cooling (finger concept, KIT)**

Approaches to CFTR Divertor Design

Phase I

Fusion Power: 50-100 MW

ITER-like Vertical Target, accommodating snowflake w/o additional coils

Phase II

Fusion Power: 400 MW

Snowflake or more advanced configuration – SXD

Phase III

Fusion Power: 800 MW

Demo-relevant Divertor, e.g., KIT, or liquid divertor

Approaches to CFTR Divertor Design

Optimize Magnetic configurations and target geometry :

1. Optimize Magnetic configurations --- physics design group
 2. Design target geometry
 3. Calculate distributions of particles and heat using SOLPS code
 4. Optimize target geometry
- 

Start engineering conceptual design:

1. Preliminary design on target, heat sink, support structure, cooling structure and cassette body...
 2. Electromagnetic analysis of the divertor components (DINA/MIT+ANSYS)
 3. Neutron volumetric heating calculations (code?)
 4. Thermo-mechanical analysis and structure analysis (ANSYS)
 5. Optimize divertor structure design
- 